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(54) Well logging method and apparatus using annular and azimuthal electrodes.

(57) The invention relates to an electrical logging method and apparatus using electrodes. The apparatus comprises an annular current electrode (A₀) mounted on a body and guard electrodes (A₂, A'₂) disposed on the body above and below the annular current electrode. A first measurement current (I₀) is emitted by the central current electrode (A₀) and focusing currents are emitted by the guard electrodes (A₂, A'₂). A first output signal representative of the deep resistivity of the formations is generated in response to the first measurement current (I₀). One of the guard electrodes (A₂) comprises two longitudinally spaced-apart portions, and an array of azimuthal current electrodes (A_{az}) that are circumferentially spaced-apart from one another is disposed between these two portions. Second measurement currents (A_{az}) emitted by the azimuthal current electrodes (A_{az}) are focused longitudinally by the currents emitted by the said two portions of the guard electrode (A₂). Second output signals are generated in response to the second measurement current (I_{az}), which output signals are representative of the resistivity of the formations in a plurality of directions around the borehole. A high resolution resistivity signal is calculated as a function of the mean of the second measurement currents (I_{az}).

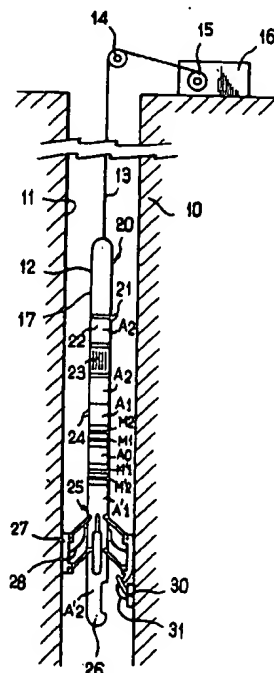


FIG. 1

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The invention relates to well logging for evaluating the resistivity of earth formations through which a borehole passer, and more particularly to an electrical logging method and apparatus using electrodes.

A well logging device with electrodes that has been commercially available for many years and that is known under the name "Dual Laterolog" is described in US patent 3 772 589 (Scholberg). That device comprises an array of annular electrodes used for sending electrical measurement currents into the formations for the purpose of measuring their resistivity. The measurement currents are focused in an annular zone having the form of a disk perpendicular to the borehole axis by means of auxiliary currents emitted by guard electrodes. That device includes measuring deep resistivity of the earth formations (LLd mode) and measuring shallower resistivity of the earth formations (LLs mode) by emitting currents at different frequencies, typically 35 Hz and 280 Hz.

A drawback of that device is that its longitudinal resolution (i.e. in the longitudinal direction of the borehole) is poor, being about one meter. In addition, in some cases and in particular in boreholes that are deviated or horizontal, the annular zone scanned by the device around the borehole comprises different layers of earth formation and gives an average measurement that has little meaning. It is therefore desirable to obtain resistivity measurements in a plurality of azimuthal directions around the borehole.

Logging apparatuses are known that detect the resistivity of formations in a plurality of azimuthal directions around the axis of the borehole. Those devices seek to obtain information about fractures or about the dip of formations. For example, British patent 928 583 (British Petroleum Company Limited) describes an array of azimuthal measurement electrodes distributed circumferentially around the periphery of a logging sonde. A guard electrode which surrounds the measurement electrodes enables an auxiliary current to be emitted for focusing the currents emitted by each of the measurement electrodes.

A difficulty with those apparatuses is obtaining effective focusing of the azimuthal measurement currents.

The radial investigation depth obtained with azimuthal electrodes is generally less than that obtained with a deep Laterolog device of known type. It is therefore desirable to provide conventional deep Laterolog measurements in addition to azimuthal resistivity measurements.

An object of the invention is to provide a technique of logging with electrodes that enables conventional type deep resistivity measurements to be obtained simultaneously with azimuthal resistivity measurements.

Such a combination of measurements poses various problems. Firstly it is desirable to retain the characteristics of conventional deep resistivity measuring apparatuses. In addition, the influence of each type of measurement on the other should be reduced to as little as possible. Finally, while retaining the quality of the focusing in deep measurement, it is important to obtain effective focusing for azimuthal measurements.

Another object of the invention is to provide a combination of deep resistivity measurements and azimuthal resistivity measurements enabling the above problems to be resolved.

Another object of the invention is to provide a technique of logging with electrodes that provides resistivity measurements with high resolution.

In a first aspect of the invention, a method of evaluating the resistivity of earth formations having a borehole passing therethrough comprises the steps of: emitting a first electrical measurement current into the formations via an annular current electrode disposed on an elongate body adapted to be moved along the borehole; focusing the first measurement current by means of auxiliary electrical currents emitted by annular guard electrodes disposed longitudinally on the body on opposite sides of the annular current electrode; and generating a first output signal representative of the resistivity of the formations in response to the first measurement current. The method further includes the steps of: using a guard electrode made with two longitudinally spaced-apart portions, emitting second electrical measurement currents into the formations via an array of azimuthal current electrodes that are spaced-apart circumferentially from one another and that are disposed on the body between said two portions; focusing the second measurement currents longitudinally by means of auxiliary electrical currents emitted by the two portions of the guard electrode; and generating second output signals representative of the resistivity of the formations in a plurality of directions around the borehole in response to the second measurement currents.

In a preferred embodiment, the first output signal is a deep resistivity signal (R_a) representative of the ratio of the potential (V_o) detected on an annular monitor electrode divided by the current (I_o) emitted by the annular current electrode. The second output signals are azimuthal resistivity signals (R_{az_i}), each of them being representative of the ratio of the potential (V_{az_i}) detected on a monitor electrode divided by the current (I_{az_i}) emitted by an azimuthal current electrode. In addition, an additional output signal (R_{br}) is generated which is a function of the sum of the azimuthal currents (I_{az_i}).

According to another aspect of the invention, apparatus for evaluating the resistivity of earth formations having a borehole passing therethrough comprises: an elongate body adapted to be displaced along the borehole; an annular current electrode mounted on the body; guard electrodes disposed on the body on opposite sides of the annular current electrode; means for emitting a first electrical measurement current via the current

electrode; means for emitting electrical focusing currents via the guard electrodes; and means responsive to the first measurement to generate a first output signal representative of the resistivity of the formations. A selected guard electrode comprises two portions that are longitudinally spaced apart from each other and an array of azimuthal current electrodes that are circumferentially spaced apart from one another is disposed between the two portions of the selected electrode. In addition, the apparatus comprises means for emitting second electrical measurement currents from the azimuthal current electrode and means for responding to the second measurement currents to generate second output signals representative of the resistivity of the formations in a plurality of directions around the borehole.

The guard electrodes preferably comprise first (A1, A'1) and second (A2, A'2) pairs of annular electrodes, the second pair of guard electrodes being disposed on opposite sides of the first pair. The selected guard electrode is then one of the electrodes in the second pair (A2, A'2). Since both portions of the selected guard electrode extend over a relatively large distance on opposite sides of the azimuthal electrodes, effective focusing of the azimuthal currents is obtained.

The characteristics and advantages of the invention appear more clearly from the following description given by way of non-limiting example and made with reference to the accompanying drawings, in which:

Figure 1 shows a logging apparatus according to the invention comprising an electrode sonde suspended in a borehole;

Figure 2 shows a configuration of azimuthal electrodes used by the Figure 1 sonde; and

Figures 3A and 3B are circuit diagrams respectively of the downhole circuits and the surface circuits in the logging apparatus of Figure 1.

With reference to Figure 1, a logging apparatus for evaluating the resistivity of earth formations 10 having a borehole 11 passing therethrough comprises a sonde 12 suspended in the borehole at the end of a multi-conductor cable 13. The cable 13 passes over a sheave 14 and is wound onto a winch 15 for moving the sonde 12 along the borehole. The winch 15 constitutes a portion of a surface unit 16.

The sonde 12 has four sections fixed end to end so as to make up an elongate body 17. The top section 20 is a sealed metal housing containing electrical circuits that are described in greater detail below. A first intermediate section 21 comprises a tubular body 22 which carries an array 23 of azimuthal electrodes that are circumferentially spaced apart from one another. A second intermediate section 24 fixed to the bottom of the first intermediate section 21 carries annular electrodes used for conventional Laterolog type measurements. A bottom section 25 comprises a metal body 26 having four centralizing shoes 27 adapted to bear against the wall of the borehole 11 under drive from leaf springs 28. A measuring shoe 30 hinged to the bottom end of one of the centralizing shoes 27 is urged by an individual spring 31 against the wall of the borehole. This measuring shoe 30 is fitted with conventional electrodes for performing conventional type spherically focused microresistivity measurements.

The sonde 12 includes a first array of annular electrodes for implementing the Dual Laterolog technique described in US patent 3 772 589 (Scholberg). As described in that patent, the intermediate section 24 carries a central electrode Ao, a first pair of monitor electrodes M1, M'1 connected to each other and disposed on opposite sides of the electrode Ao, a second pair of monitor electrodes M2, M'2 disposed on opposite sides of the pair M1, M'1, and a first pair of guard electrodes A1, A'1 that are connected to each other and are disposed on opposite sides of the pair M2, M'2. The sonde also includes a second pair of guard electrodes A2, A'2 that are connected to each other, with the guard electrode A2 being formed by the body 22 of the intermediate section 21 and with guard electrode A'2 being formed by the body 26 of the bottom section 25.

In the Dual Laterolog technique, the resistivity of the formations at two different radial investigation depths are measured by sending electrical currents at two different frequencies f1 and f2. For the shallow measurement (LLs mode) an alternating measurement current is emitted at a first frequency f1 (e.g. 280 Hz) by the central electrode Ao, said measurement current being focused by an auxiliary current sent between the pair of electrodes A1, A'1 and the pair of electrodes A2, A'2. For further details, reference may be made to the above-mentioned Scholberg patent.

For the deep measurement in LLd mode, an alternating current is used at a low frequency f2 (e.g. 35 Hz) likewise emitted by the electrode Ao. This measurement current is focused by same-frequency auxiliary currents emitted both by the electrodes A1, A'1 and A2, A'2. The auxiliary currents are controlled by a feedback loop circuit that maintains the potential difference between the two pairs of electrodes M1, M'1 and M2, M'2 at substantially zero. The measurement current is thus maintained in a zone which is disk-shaped and perpendicular to the axis of the borehole. This prior technique is used by the apparatus of the invention for obtaining LLd type measurement signals. A portion of the circuits shown in Figures 3A and 3B performs the functions required for such LLd mode measurement.

In addition to the electrodes enabling it to perform conventional LLd and LLs mode measurements, the apparatus of Figure 1 includes an array 23 of azimuthal electrodes and other electrodes shown in greater detail

in Figure 2.

Figure 2 shows the intermediate section 21 of the sonde. The metal tubular body 22 of this section forms an electrode A2 that has a top portion and a bottom portion. Between the two portions of the electrode A2 an isolated central section carries a pair of annular monitor electrodes M3 and M4 that are electrically connected together. Between the two annular electrodes M3 and M4, there is an array 23 of twelve azimuthal current electrodes Aaz_i that are spaced apart circumferentially from one another, where i is an index in the range 1 to 12. Each of the azimuthal current electrodes is substantially rectangular in shape being elongate in the longitudinal direction, is insulated from the body, and surrounds an azimuthal monitor electrode Maz_i. Each azimuthal monitor electrode Maz_i is insulated both relative to the body and relative to the electrode Aaz_i that surrounds it. It too is substantially in the form of a rectangle and it extends over nearly the entire length of the associated current electrode.

In the embodiment described the annular monitor electrodes M3 and M4 are situated between the portions of the electrode A2 and the array 23 of azimuthal electrodes. These monitor electrodes could also be situated within each portion of the electrode A2 so that the top portion of the electrode A2 extends below the electrode M4 and the bottom portion of the electrode A2 extends above the electrode M3.

To obtain resistivity measurements in a plurality of directions around the borehole, electrical currents are emitted into the formations from the azimuthal current electrodes Aaz_i. These currents are focused longitudinally and azimuthally by an active feedback loop system or servo-control system that includes the azimuthal monitor electrodes Maz_i, the annular monitor electrodes M3 and M4, and the two portions of the guard electrode A2. For longitudinal focusing, an auxiliary current is emitted by the electrode A2. In addition, the system for servo-controlling the azimuthal measurement currents provides mutual azimuthal focusing between the currents.

It has been found that the passive focusing of prior art devices can be highly disturbed by the differences in electrode contact impedance. In previously described apparatuses where azimuthal electrodes are used, the survey current electrodes and the guard electrodes are maintained at the same potential for focusing the measurement currents. When the electrodes are immersed in the fluid of the borehole, it is observed that the contact impedances of these electrodes can be very different from one another. While current is being emitted, the potential of a current electrode is no longer equal to the potential of the borehole fluid facing it but is of a potential that includes an error which is a function of the product of the emitted current multiplied by the contact impedance. This error in the potential of the current electrode may degrade the focusing of the measurement current. This phenomenon is particularly troublesome with a plurality of measurement currents that are circumferentially directed around the borehole axis.

In the apparatus of Figures 1 and 2, emission of the azimuthal measurement currents Iaz_i is so controlled as to maintain the potential difference between each azimuthal monitor electrode Maz_i and the set of electrically interconnected annular monitor electrodes M3, M4 at substantially zero. The azimuthal resistivity measurements are obtained by taking the ratios Vaz_i/Iaz_i of the potential Vaz_i of one of the annular monitor electrodes M3, M4 divided by the azimuthal measurement currents Iaz_i. In the general case, each azimuthal resistivity measurement is a function of the ratio of the potential detected on an azimuthal monitor electrode Maz_i divided by the current emitted by the associated azimuthal current electrode Aaz_i. In the example described, the potential Vaz_i may be detected on any one of the monitor electrodes Maz_i, M3, or M4.

The downhole and the surface circuits of the apparatus are shown diagrammatically in Figures 3A and 3B.

With reference to Figure 3A, the downhole circuits are situated in sections 20 and 21. The above-described electrodes are shown diagrammatically on the right of the figure, with only one electrode Maz_i and only one electrode Aaz_i being shown in order to simplify the description.

In alternating current It at a frequency of 35 Hz is sent by one or more conductors 40 of the cable 13 from the surface to the downhole sonde. This total current It is detected downhole by means of a low resistance series resistor 41 whose terminals are connected to an amplifier 42 followed by a bandpass filter 43 centered on the frequency of 35 Hz. The phase of the total current It is also detected by means of a phase detector circuit 44. Downhole measurement of the total current It and detection of its phase make it possible to ignore any distortion that may have been introduced by transmission along the cable 13. A portion of the total current is applied via a conductor 45 to the electrodes A2 and A'2 that are electrically interconnected by very low resistance copper bars 46. As explained below, the total current flows between the current electrodes and a remote electrode B situated on the surface.

The apparatus includes circuits used for operating in LLs mode with an alternating current at 280 Hz. These circuits are not shown in Figure 3A in order to simplify the description. The person skilled in the art will have no difficulty in adding such circuits to Figures 3A and 3B given the detailed description thereof provided in the above-mentioned Scholberg patent. In conventional manner, these circuits provide a shallow resistivity signal

which is recorded on the surface at a function of depth. The present description is therefore limited to describing the circuits that operate in low frequency mode at 35 Hz.

A portion of the circuits shown in Figure 3A is devoted to conventional LLd mode measurement.

A feedback loop keeps the potential difference between the pairs of monitor electrodes M1, M'1 and M2, M'2 at substantially zero so as to focus the measurement current emitted by the electrode no. The monitor electrodes M1 and M2 are connected to a first primary winding of a differential transformer 50, and the monitor electrodes M'1 and M'2 are connected to a second primary winding of the same transformer. The secondary winding of the transformer 50 is connected to the inputs of a broad band filter circuit 51 having high gain amplification and having its output applied to the primary winding of a transformer 52. One end of the secondary winding of the transformer 52 is connected to the electrode Ao and the other end thereof is connected to one of the primary winding of a measurement transformer 53 whose other end is connected to the guard electrodes A1, A'1 which are short-circuited together by a copper bar 54. The secondary of the measurement transformer 53 is connected to an amplifier 55 whose output is applied to a bandpass filter centered on the frequency of 35 Hz. The output of the filter 56 provides an alternating signal representing the current I_o emitted by the electrode Ao.

Another feedback loop short circuits the guard electrodes A1, A'1 and A2, A'2 at the frequency of 35 Hz. A pair of interconnected monitor electrodes A1*, A'1* is disposed in the vicinity of the guard electrodes A1, A'1. Another pair of interconnected monitor electrodes is disposed in the vicinity of the guard electrodes A2, A'2. These two pairs of electrodes are connected to the input of a high gain differential amplifier circuit 60 including a filter function at the frequency 35 Hz and having its output applied to the primary winding of a transformer 61. The secondary winding of the transformer 61 is connected between the guard electrode A'1 and the guard electrode A'2.

One of the monitor electrodes M1 or M2, in this case M2, is connected to the input of a measurement amplifier 62 whose other input is connected to the armor of the cable which serves as a remote reference electrode N. The output of the amplifier 62 is applied to a bandpass filter 63 centered on the frequency of 35 Hz and whose output provides an alternating signal corresponding to the potential difference V_o between the electrode M2 and the electrode N.

The above-described circuits perform the functions required for the LLd operating mode as described in the Scholberg patent.

The apparatus shown in Figure 3A also includes circuits for generating azimuthal resistivity signals. The short-circuited annular monitor electrodes M3 and M4 are connected to the input of a measurement amplifier 64 whose other input is connected to the reference electrode N on the cable armor. The output of the amplifier 64 is applied to a bandpass filter centered on the frequency of 35 Hz which provides an alternating signal V_{az_i} representative of the potential difference between the electrodes M3, M4 and the reference electrode N.

Each azimuthal monitor electrode M_{az_i} is connected to the input of a high gain differential amplifier circuit 68_i which also includes a filter function at 35 Hz. The other input of each circuit 68_i is connected to the annular monitor electrodes M3, M4 and its output is applied to a current source 69_i constituted by a voltage-current converter. The output current from the source 69_i is applied between the guard electrode A2 and the azimuthal current electrode A_{az_i} corresponding to the monitor electrode M_{az_i} under consideration. This loop controls each of the azimuthal currents I_{az_i} in such a manner as to maintain the potential difference between M3, M4 and the corresponding azimuthal monitor electrode at zero.

The output signal from the circuit 68_i is also applied to a measurement amplifier 70_i followed by a bandpass filter 71_i centered on the frequency of 35 Hz so as to provide an alternating signal I_{az_i} representative of the measurement current emitted by the azimuthal electrode A_{az_i} . As shown in dashed lines in Figure 3A, the apparatus has twelve identical channels providing the measurement currents I_{az_i} .

The signals I_o , V_o , V_{az_i} , I_t , and the twelve signals I_{az_i} are applied to a multiplexer 73 whose output is applied to a variable gain amplifier 74 and then to an analog-to-digital converter 75. The digital outputs from the converter 75 are applied to a digital processor circuit 76 constituted by a digital signal processor (DSP) programmed to perform a phase sensitive detector (PSD) function and a lowpass filter function. The phase reference required for the detector function comes from the circuit 44 so as to be synchronized with the total downhole current I_t . The processor circuit 76 also provides a control signal to the variable gain amplifier 74 so as to reduce the dynamic range of the input signals to the analog-to-digital converter 75.

The multiplexed digital signals representing the amplitudes of the currents or voltages I_o , V_o , V_{az_i} , I_t and I_{az_i} are applied to remote measurement circuits 77 for modulating and transmitting the signals to the surface via the cable 13.

As shown in Figure 3B, the downhole signals are received and demodulated at the surface by a remote measurement circuit 80 and they are then input to a computer 81 which may be a Microvax microcomputer as sold by Digital Equipment Corporation, for example. The computer 81 demultiplexes the signals I_o , V_o , V_{az_i} ,

It, and Iaz_i , and it calculates formation resistivity signals Ra , Rs , Raz_i , and Rhr , using the following equations:

$$Ra = k_1 \cdot Vo/Io$$

$$Rs = k_2 \cdot Vo/It$$

$$Raz_i = k_3 \cdot Vaz_i/Iaz_i$$

$$5 \quad Rhr = k_4 \cdot Vaz_i/\Sigma Iaz_i$$

in which k_1 , k_2 , k_3 , and k_4 are predetermined constants that depend on the geometry of the downhole sonde. Ra is the LLD type deep resistivity measurement; Rs is the resistivity measurement of the surrounding formations; Raz_i are twelve azimuthal measurements of resistivity around the borehole; and Rhr which corresponds to a mean of the conductivity $1/Raz_i$ is a measure of formation resistivity having high longitudinal resolution.

10 These various resistivity signals are recorded as a function of depth in a recording apparatus 82 which may comprise as optical recorder and a magnetic recorder. Prior to recording, the signals Raz_i and Rhr are depth corrected in conventional manner to take account of the fact that they are obtained on the downhole sonde at a different depth from the signal Ra and Rs .

15 A 35 Hz current source 83 delivers the total current It via one or more conductors of the cable 13 and a return electrode B placed on the surface of the ground. The current It is controlled by means of a variable gain amplifier which receives a control signal from the computer 81. The control signal is designed to minimize the dynamic range of the measurement signals. One example of minimizing is given in the Scholberg patent which maintains the product $Vo \cdot Io$ constant.

20 The embodiment described above may naturally be varied or improved in numerous ways while remaining within the scope of the invention as defined in the following claims. In particular, the array of azimuthal electrodes may be combined with other logging apparatuses focused by annular electrodes, such as, for example, a Laterolog 3, a Laterolog 9, or a spherical focusing type apparatus.

25 Claims

1. A method of evaluating the resistivity of earth formations having a borehole passing therethrough, the method comprising the steps of:
 - 30 emitting a first electrical measurement current (I_o) into the formations via an annular current electrode (A_o) disposed on an elongate body adapted to be moved along the borehole;
 - focusing the first measurement current by means of auxiliary electrical currents emitted by guard electrodes ($A2$, $A'2$) disposed longitudinally on the body on opposite sides of the annular current electrode, a selected one of said guard electrodes ($A2$) having two longitudinally spaced-apart portions;
 - 35 generating a first output signal representative of the resistivity of the formations in response to the first measurement current (I_o);
 - emitting second electrical measurement currents (Iaz_i) into the formations via an array of azimuthal current electrodes (Aaz_i) that are spaced-apart circumferentially from one another and that are disposed on the body between the two portions of said selected guard electrode ($A2$);
 - 40 focusing the second measurement currents (Iaz_i) longitudinally by means of auxiliary electrical currents emitted by the two portions of the selected guard electrode ($A2$); and
 - generating second output signals representative of the resistivity of the formations in a plurality of directions around the borehole in response to the second measurement currents (Iaz_i).
2. A method according to claim 1, wherein the step of focusing the first measurement current comprises emitting auxiliary electrical currents via a first pair ($A1$, $A'1$) and a second pair ($A2$, $A'2$) of guard electrodes, the second pair of guard electrodes being disposed on opposite sides of the first pair, and wherein the selected guard electrode is one of the electrodes ($A2$) of the second pair.
3. A method according to claim 1 or 2, wherein the step of focusing the first measurement current comprises the steps of:
 - 50 detecting the potential difference that appears between a first pair ($M1$, $M'1$) and a second pair ($M2$, $M'2$) of annular monitor electrodes disposed on the body between the annular current electrode (A_o) and the guard electrodes; and
 - controlling the emission of auxiliary currents in such a manner as to maintain the detected potential difference at substantially zero.
 - 55
4. A method according to claim 3, wherein the step of generating the first output signal comprises generating a deep resistivity signal (Ra) as a function of the ratio (Vo/I_o) of the potential (Vo) detected on an annular

monitor electrode (M1, M'1, M2, M'2) divided by the current (I_o) emitted by the annular current electrode.

- 5 5. A method according to any one of claims 1 to 4, wherein the step of generating the second output signals comprises generating an azimuthal resistivity signal (R_{az_i}) for each azimuthal current electrode (A_{az_i}), each azimuthal resistivity signal being a function of the ratio (V_{az}/I_{az_i}) of the potential (V_{az}) detected on a monitor electrode (M3, M4) divided by the current (I_{az_i}) emitted by one of the azimuthal current electrodes.
- 10 6. A method according to claim 5, further including the step of generating an additional output signal (R_{hr}) as a function of the sum of the currents (I_{az_i}) emitted by the azimuthal electrodes.
- 15 7. Apparatus for evaluating the resistivity of earth formations having a borehole (11) passing therethrough, the apparatus comprising:
 - an elongate body (17) adapted to be displaced along the borehole;
 - an annular current electrode (A_o) mounted on the body;
 - guard electrodes ($A_2, A'2$) disposed on the body on opposite sides of the annular current electrode (A_o);
 - means (50, 51, 52) for emitting a first electrical measurement current (I_o) via the current electrode (A_o);
 - means (60, 61) for emitting electrical focusing currents via the guard electrodes ($A_2, A'2$); and
 - 20 means (81) responsive to the first measurement current (I_o) to generate a first output signal representative of the resistivity of the formations;
 - the apparatus being characterized in that a selected one of said guard electrodes (A_2) comprises two longitudinally spaced-apart portions;
 - and in that the apparatus comprises:
 - 25 an array (23) of azimuthal current electrodes (A_{az_i}) that are circumferentially spaced-apart from one another and disposed between the two portions of the selected electrode (A_2);
 - means (68, 69) for emitting second electrical measurement currents (I_{az_i}) from the azimuthal current electrodes (A_{az_i}); and
 - means (81) responsive to the second measurement currents (I_{az_i}) to generate second output signals representative of the resistivity of the formations in a plurality of directions around the borehole.
- 30 8. Apparatus according to claim 7, characterized in that it includes a first pair ($A_1, A'1$) and a second pair ($A_2, A'2$) of guard electrodes, the second pair of guard electrodes being disposed on opposite sides of the first pair, the selected guard electrode being one of the electrodes (A_2) of the second pair.
- 35 9. Apparatus according to claim 8, characterized in that the selected guard electrode is the upper electrode (A_2) of the second pair.
- 40 10. Apparatus according to any one of claims 7 to 9, characterized in that said means for emitting the focusing currents comprise:
 - a first pair ($M_1, M'1$) and a second pair ($M_2, M'2$) of annular monitor electrodes disposed on the body between the annular current electrodes (A_o) and the guard electrodes; and
 - means (50, 51, 52) for maintaining the potential difference detected between the first pair ($M_1, M'1$) and the second pair ($M_2, M'2$) of monitor electrodes at substantially zero.
- 45 11. Apparatus according to claim 10, characterized in that said means for generating the first output signal comprise:
 - means (62, 63) for detecting the potential (V_o) on one of the annular monitor electrodes ($M_1, M'1, M_2, M'2$);
 - means (53, 55, 56) for detecting the current (I_o) emitted by the annular current electrode (A_o); and
 - 50 means (81) for generating a deep resistivity signal (R_a) as a function of the ratio (V_o/I_o) of the detected potential (V_o) divided by the detected current (I_o).
- 55 12. Apparatus according to any one of claims 7 to 11, characterized in that said means for generating the second output signals comprise:
 - means (64, 65) for detecting the potential (V_{az_i}) that appears on a monitor electrode (M_3, M_4);
 - means (70, 71) for detecting the currents (I_{az_i}) emitted by each azimuthal current electrode (A_{az_i});
 - and
 - means (81) for generating azimuthal resistivity signals (R_{az_i}) each of which is a function of the ratio

(V_{azi}/I_{azi}) of the detected potential (V_{azi}) divided by the detected azimuthal current (I_{azi}) emitted by one of the azimuthal current electrodes.

- 5 13. Apparatus according to claim 12, characterized in that it further includes means (81) for generating an additional output signal (R_{hr}) as a function of the sum of the detected azimuthal currents (I_{azi}).

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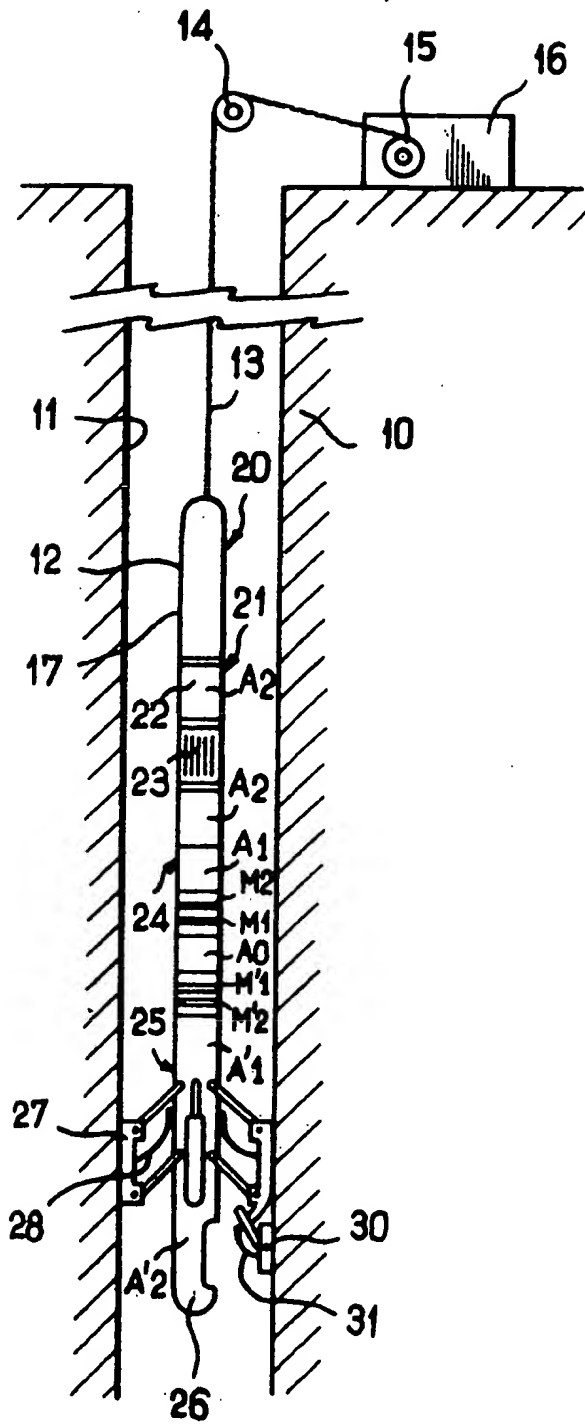


FIG. 1

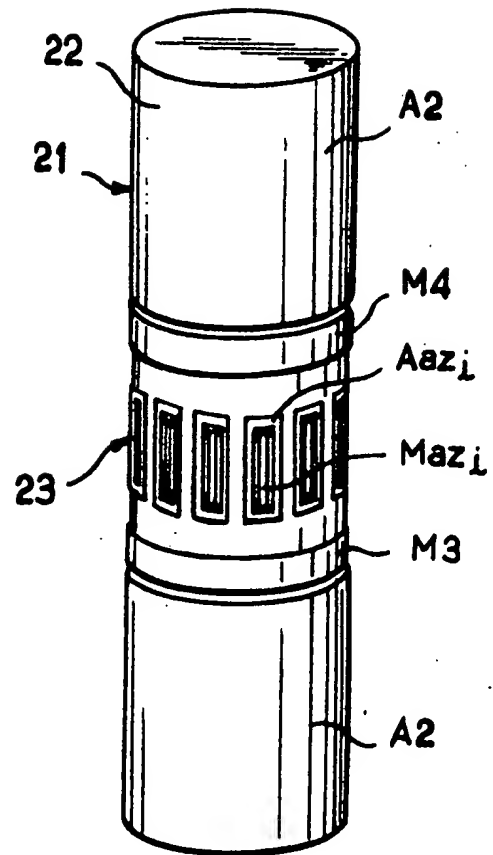


FIG. 2

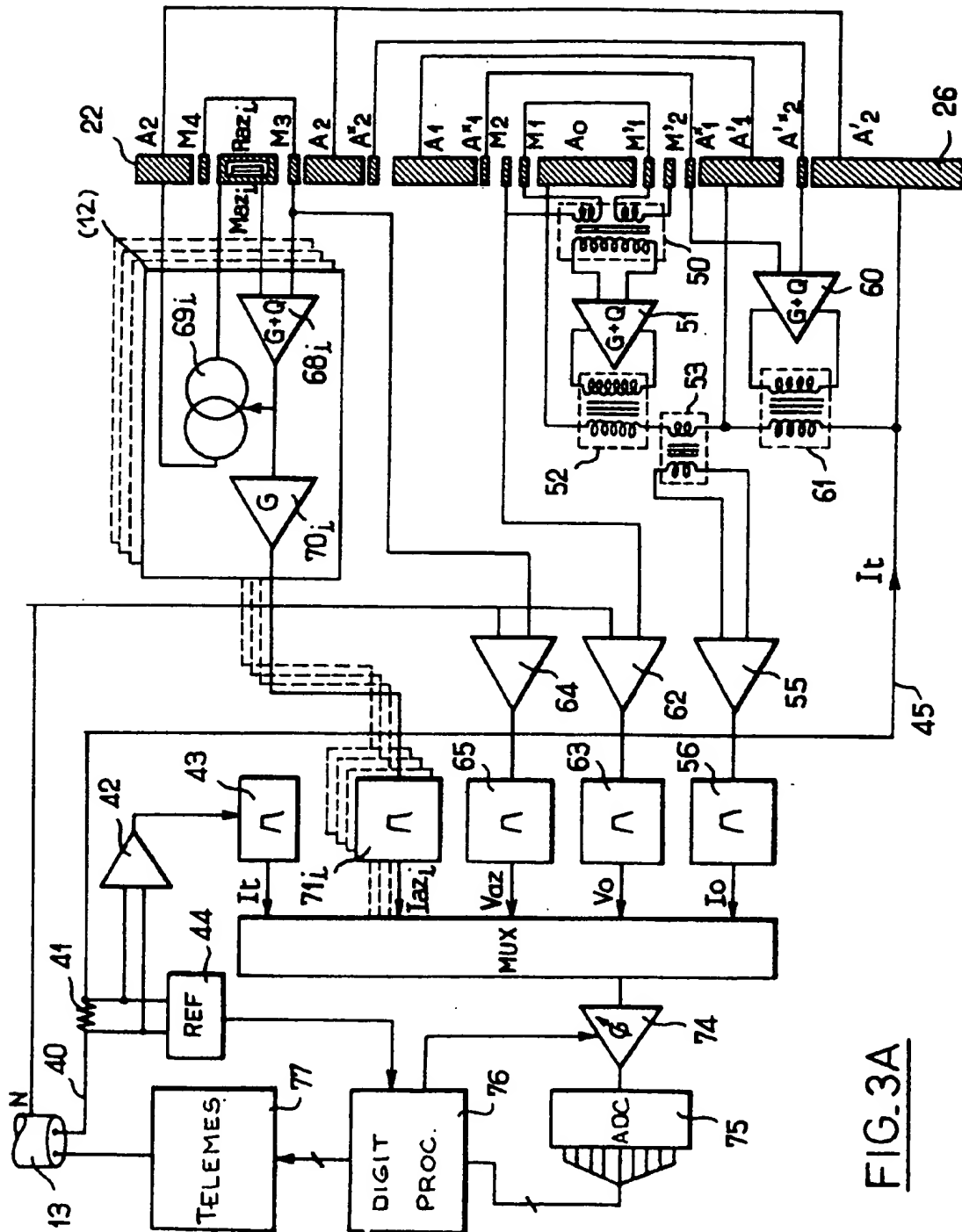
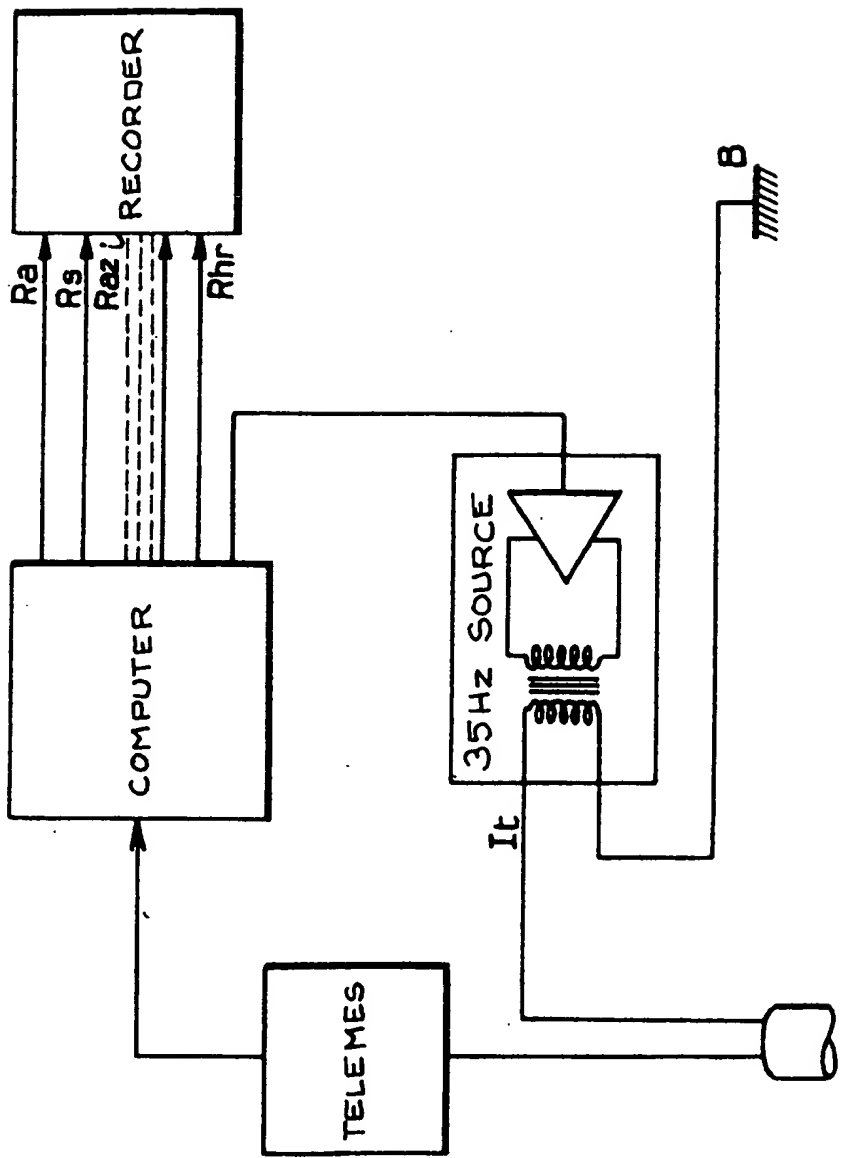


FIG. 3B





European Patent
Office

EUROPEAN SEARCH REPORT

Application Number

EP 92 40 3161

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
A	CA-A-941 014 (D.T.OWER) * claims 1,6-11,19,23,26,28,38-40; figures 8-10 *	1,7	G01V3/24
A	US-A-3 075 142 (J.C.ALBRIGHT E.A.) * column 2, line 8 - line 18 * * column 3, line 70 - line 75 * * column 5, line 30 - line 54 * * claims 1,4; figure 1 *	1	
A	US-A-3 136 942 (N.A.SCHUSTER) * column 9, line 63 - column 10, line 46 *	1	
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			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			G01V
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 10 MARCH 1993	Examiner HAASBROEK J.N.
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